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THE BREAKING STRENGTH AND EXTENSION OF WEATHERED RUBBER-COATED --ETC(U)
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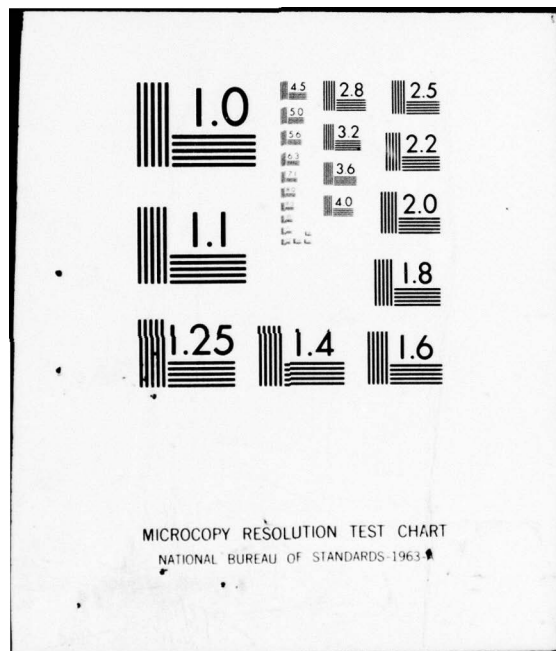
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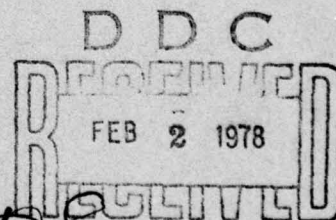
**THE BREAKING STRENGTH
AND EXTENSION OF WEATHERED
RUBBER-COATED FABRICS**

by

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M. Webb

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Procurement Executive, Ministry of Defence
Farnborough, Hants

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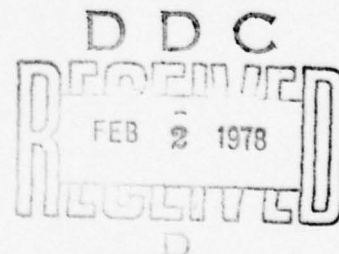
11 Mar 7712 22p.6 THE BREAKING STRENGTH AND EXTENSION OF WEATHERED RUBBER-COATED FABRICS.
by10 J. E. Swallow
M. WebbSUMMARY

The breaking strength and extension of a nylon and of a cotton fabric, each coated with natural rubber, neoprene, polyurethane or chlorosulphonated polyethylene and exposed to various weathering conditions, were determined. Although the coated nylon fabrics were stronger and more extensible than the cotton ones, those with natural rubber coating deteriorated at a faster rate when exposed under load. Nylon coated with polyurethane was initially stronger and more extensible than when coated with the other rubbers, but in hot moist weathering conditions deteriorated faster. Extension was more severely affected than strength by load during exposure.

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1 INTRODUCTION

The exposure of rubber-coated fabrics for up to one year of weathering and the effects of this on their flexibilities have previously been reported¹. In a collaborative trial involving several Establishments of MOD(PE) and JTRU, nylon and cotton base fabrics of similar mass per unit area were coated with natural, neoprene, polyurethane (PU) or chlorosulphonated polyethylene (CSPE) rubbers. These coated fabrics were exposed for periods of three, six or twelve months, and a second period of six months (6S) commencing at the end of the first, under loads of 1% or 10% of the nominal breaking strength. Pieces of fabric were positioned at 45° to the horizontal and facing the equator at a site in the UK (ERDE, Waltham Abbey) and at two sites in Queensland (hot, dry at Cloncurry and hot, wet, cleared jungle at Innisfail).

The coated nylon fabrics were found to be thicker, heavier and less flexible than the coated cotton fabrics; PU rubber, particularly on nylon, stiffened more than the other rubbers during exposure.

The present Report gives the results and their analyses for the breaking strength and extension of these coated fabrics on weathering.

2 DETERMINATION OF BREAKING STRENGTH AND EXTENSION

Strengths and extensions were determined in accordance with standard test methods². Rectangular warpway strips of coated fabric, 30 cm long × 5 cm wide and cut from the exposed specimens¹, were positioned in a tensile testing machine so as to have a gauge length of 20 cm. These lengths were then broken in approximately 60 s at constant rate of traverse, the load-extension curves being recorded. The machine was situated in a room at 20°C and 65% relative humidity, and the fabric strips were conditioned in this atmosphere for at least 24 h before testing. Two test pieces were available from each specimen.

3 ARRANGEMENT OF RESULTS

The results are given in Tables 1 and 2. They were obtained by three operators and were inevitably separated in time of determination by well over a year. All the measurements of extension were made by one operator (JES) from the load-extension curves obtained by the three operators. For a discussion of the effect of these on the errors, see section 4.1.

As noted previously¹, the three month specimens from Australia were not differentiated as to their loading conditions. It was therefore assumed that
031 the columns containing the lower nylon/natural rubber strengths should be

ascribed to the 10% loading in accord with the lower strengths found for this combination at the longer times where the specimens were differentiated. If this unverifiable assumption were incorrect, or if some of the results in one column properly belonged to the other, the main effect would be an inflation of errors rather than reversed conclusions, and set (b) below might be expected to contain anomalous results.

Out of the 192 exposed specimens, 12 broke during exposure and of these five were lost. The results could not therefore be analysed in terms of the original five-factor design. They were consequently divided into nine complete four-factor sub-experiments, though 12 of the combinations for which results were available could not be used. The remaining 368 values were analysed by computer using sets containing the following columns from Tables 1 and 2:

Set	No. of columns in set	Columns from Tables 1 & 2 used	No. of columns determined by operator			Brief description ¹
			JES	MW	BM	
(a)	2	A,B	1	1	0	Controls
(b)	6	C,D,K,L,S,T	0	6	0	3 months
(c)	12	C,E,G,I,K,M,O,Q,S,U,W,Y	5	4	3	1%
(d)	24	C-Z	10	8	6	Natural rubber
(e)	8	C-J	4	4	0	ERDE
(f)	6	A,B,C,E,G,I	3	3	0	ERDE, 1%, with controls
(g)	6	A,B,K,M,O,Q	4	2	0	Cloncurry, 1%, with controls
(h)	6	A,B,S,U,W,Y	1	2	3	Innisfail, 1%, with controls
(i)	24	C-Z	10	8	6	Nylon with three rubbers

4 RESULTS AND DISCUSSION

4.1 Analysis of errors

The error variances are given in Table 3. In general, sets (i) and (h) had greater random variability than the others; in particular, (i) was more variable than (b), (e) and (g) at about the 99.9% level of probability. It is possible

that the external factors comprising the columns in these sets gave rise to more random variability than the internal factors comprising the rows. The columns also included more potential effects due to operator, and to time between performing the tests, since these effects were confounded with columns and not with rows.

The set means and coefficients of variation are also given in Table 3. These coefficients were comparable in magnitude with those for bending length¹.

4.2 Breaking strength and extension

4.2.1 General

Analysis of variance within each set is given for breaking strength in Table 4 and for breaking extension in Table 5. Certain interactions were directly determinate in each set, and comparisons between sets gave some additional indirect indication of interactions.

The effects are discussed below in roughly their order of importance. In general, only those which reached the 99.9% level of probability of being correct assertions are considered. The significant means are given in Tables 6 and 7, though where means were found to be significant in one set they are given for all the others in which they were determinate even though they may not have then been found to be significant.

4.2.2 Effect of fabric (F)

This had variance ratios of upwards of 1500; not surprisingly, the coated nylon fabrics were shown to be stronger and more extensible than the cotton ones. The strength ratio was 3.4 in the controls, falling to an average of 2.5 in the weathered sets. The extension ratio was 2.4 in the controls and an average of 2.6 in the others.

4.2.3 Effect of load (L)

The exposures at 10% load were more damaging than those at 1%. For this factor, the variance ratios for extension were consistently higher than those for strength. In sets (d) and (i) the variance ratios for strength were more than 100, and the strength retained under the higher load fell in set (d) to only 0.75 of that under the lower load. In all cases where determination was possible, the variance ratios for extension were more than 300, and the extension retained under the higher load fell in set (d) to only 0.63 of that under the lower load.

4.2.4 Fabric X load interaction (FL)

The 10% loading caused more strength loss on coated nylon fabrics than on the cotton ones, especially in set (d) (of the FRL interaction).

4.2.5 Effect of rubber (R)

The fabrics were stronger and more extensible when coated with PU than with the other types of rubber, except in set (h) where the interaction with site (Innisfail) reduced the values for the PU coated fabrics. Such an effect at the hot moist site has been noted before^{1,3}.

4.2.6 Effect of time (T)

The coated fabrics lost strength and extension with time, though except in set (d) this did not become significant until after three months. The 6- and 6S-month results were generally similar to each other. There was some indication that the final controls were stronger and more extensible than the originals. This would be consistent with some other work on the effects of storage³, but it could have been an operator effect since this was confounded with time in set (a).

4.2.7 Effect of site (S)

The Australian sites were usually more damaging than the one at ERDE. There was an indication of more strength and extension loss at Innisfail than at Cloncurry, which can probably be attributed mainly to the effect on the PU coated fabrics at Innisfail.

4.2.8 Rubber X load interaction (RL)

At 10% load, fabrics coated with natural rubber lost more strength and extension than the other fabrics.

4.2.9 Fabric X rubber X load interaction (FRL)

The natural rubber coated nylon fabric at 10% load lost more strength and extensibility than did the other combinations. This supports the observation concerning the FL interaction in set (d), where the fabrics were coated with natural rubber. It may be noted that although the FL interaction did not affect the extension, the FRL interaction was of similar magnitude for both strength and extension.

4.2.10 Fabric X rubber interaction (FR)

There was evidence in several sets that nylon/PU lost less, and nylon/neoprene more, strength than the other combinations. By comparing sets, the FR interaction appeared to be site dependent although the FRS interaction was not significant; however, it could only be directly tested in sets (b) and (c) where only short times or low loads were experienced. Although the variance ratios for extension were lower than for strength, there was some evidence from set (e) that nylon/PU lost less extension than expected.

4.2.11 Fabric X site interaction (FS)

The coated nylon fabrics lost more strength at the Australian sites than at ERDE, which supports the comparisons between sets (f), (g) and (h) for the F effect. The effect of the FS interaction on extension was not clear.

4.2.12 Fabric X time interaction (FT)

The strength ratio for the nylon to the cotton coated fabrics fell with time, the lowest found being 2.2 after twelve months at Cloncurry. The effect of the FT interaction on extension was not clear.

4.2.13 Rubber X time interaction (RT)

The results for natural rubber coated fabrics were comparatively worse at twelve months than at the other times, though this was only found to be of any noticeable importance in set (e).

4.2.14 Rubber X site interaction (RS)

The PU coated fabrics fared comparatively badly at Innisfail in set (c). This confirms the indirect indications of this interaction noted above. In the only other sets in which this interaction could be directly tested it was non-significant: these were (i) which did not include PU, and (b) which was for short times.

4.2.15 Load X site interaction (LS)

This was of minor importance. In set (i) the Cloncurry results at 10% load were perhaps lower than expected.

4.2.16 Other interactions

The other interactions which could be tested, though usually only in one or two sets, were: TS, FRT, FRS, FTL, FTS, RTL, RTS, TLS, FRTL, FRTS, FRLS, FTLS and RTLS, but in no case were they found to be of particular importance.

5 CONCLUSIONS

- (1) The breaking strength and extension of nylon and cotton fabrics of similar mass per unit area and coated with natural, neoprene, PU or CSPE rubbers have been determined after exposure to weathering in UK or Australia for up to one year under a load of 1% or 10% of the nominal breaking load.
- (2) The strength ratio for the nylon to the cotton coated fabrics was originally 3.4, but the nylon fabrics were more affected by weathering and the ratio fell to an average of 2.5, and in the Australian desert to 2.2. The extension ratio was about 2.5, with no clear effects of weathering.
- (3) The higher load had a greater effect than the lower, particularly on the extension. The lowest overall strengths and extensions were obtained for natural rubber coated fabrics: these ratios for high to low load were 0.75 for strength and 0.63 for extension.
- (4) Fabrics coated with PU were stronger and more extensible than those coated with the other rubbers, by about 10 to 20%, except at the hot, wet Australian site.

Acknowledgments

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Table 1
BREAKING STRENGTH, KN, OF WEATHERED COATED FABRICS

Site	Controls		EMDE												Cloncurry												Immisfall															
	Initial	Final	3			6			12			6S			3			6			12			6S			3			6			12			6S						
Time, months			1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10	1	10				
Load, level X																																										
Column	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V	W	X	Y	Z																
Fabric																																										
Nylon	1.41	1.38	1.38	1.00	1.17	0.80	1.06	0.60	1.08	0.88	1.20	0.90	1.21	0.72	1.02	0.56	1.14	0.69	1.27	1.01	1.17	0.93	1.02	0.60	1.08	0.67	1.27	1.01	1.17	0.93	1.02	0.60	1.08	0.67	1.27	1.01	1.17	0.93	1.02	0.60		
Natural	1.30	1.27	1.40	0.98	1.28	0.83	0.92	0.62	1.32	0.89	1.38	0.85	1.17	0.77	0.90	0.57	1.22	0.67	1.19	0.94	1.13	0.74	1.05	0.58	1.12	0.82	1.19	0.94	1.13	0.74	1.05	0.58	1.12	0.82	1.19	0.94	1.13	0.74	1.05	0.58		
Nylon	1.24	1.27	1.19	1.30	1.17	1.25	1.08	1.31	1.32	1.30	1.27	1.24	1.24	1.07	0.77	0.97	1.26	1.09	1.24	1.26	0.95	1.03	0.76	0.85	0.99	1.16	1.24	1.26	0.95	1.03	0.76	0.85	0.99	1.16	1.24	1.26	0.95	1.03	0.76	0.85		
Neoprene	1.17	1.17	1.30	1.23	1.26	1.17	1.09	1.27	1.21	1.24	1.11	1.18	1.21	1.22	0.89	0.79	1.25	0.82	1.19	1.16	1.05	1.14	0.95	1.16	1.06	1.12	1.19	1.16	1.05	1.14	0.95	1.16	1.06	1.12	1.19	1.16	1.05	1.14	0.95	1.16		
Nylon	1.37	1.47	1.43	1.45	1.36	1.43	1.34	1.26	1.46	1.44	1.42	1.37	1.32	(1.39)	1.25	(1.21)	1.35	-	1.37	1.33	1.12	1.14	1.05	-	1.03	(1.35)	1.37	1.33	1.12	1.14	1.05	-	1.03	(1.35)	1.37	1.33	1.12	1.14	1.05	-	1.03	
PU	1.37	1.37	1.41	1.41	1.34	1.43	1.45	1.37	1.40	1.38	1.35	1.35	1.32	(1.33)	1.21	(1.24)	1.37	-	1.40	1.41	0.82	1.12	0.93	-	1.05	(1.32)	1.40	1.41	0.82	1.12	0.93	-	1.05	(1.32)	1.40	1.41	0.82	1.12	0.93	-	1.05	
Nylon	1.30	1.36	1.34	1.33	1.21	1.03	1.20	1.24	1.27	1.22	1.12	1.03	1.10	1.14	1.08	0.57	1.16	1.22	1.26	1.24	0.86	1.07	1.04	0.94	1.12	0.98	1.26	1.24	0.86	1.07	1.04	0.94	1.12	0.98	1.26	1.24	0.86	1.07	1.04	0.94		
CSPE	1.33	1.39	1.27	1.33	1.17	1.19	1.22	1.33	1.32	1.15	1.18	1.12	1.16	1.14	1.00	0.80	1.20	1.18	1.31	1.26	1.06	1.03	0.98	1.09	1.10	1.15	1.31	1.26	1.06	1.03	0.98	1.09	1.10	1.15	1.31	1.26	1.06	1.03	0.98	1.09	1.10	
Cotton	0.44	0.48	0.43	0.48	0.39	0.34	0.18	0.16	0.37	0.43	0.47	0.47	0.52	0.51	0.40	0.43	0.48	0.52	0.43	0.49	0.47	0.47	0.45	0.44	0.42	0.34	0.43	0.49	0.47	0.47	0.45	0.44	0.42	0.34	0.43	0.49	0.47	0.45	0.44	0.42		
Natural	0.36	0.50	0.47	0.43	0.40	0.35	0.17	0.13	0.43	0.50	0.47	0.47	0.48	0.49	0.39	0.48	0.47	0.49	0.46	0.43	0.43	0.27	0.44	0.35	0.42	0.36	0.46	0.43	0.43	0.27	0.44	0.35	0.42	0.36	0.46	0.43	0.27	0.44	0.35	0.42		
Cotton	0.38	0.55	0.49	0.52	0.51	0.51	0.53	0.60	0.55	0.60	0.51	0.48	0.53	(0.47)	0.52	-	0.53	0.60	0.53	0.51	0.48	0.18	0.41	(0.44)	0.47	0.38	0.44	0.54	0.51	0.48	0.48	0.41	(0.44)	0.47	0.38	0.44	0.54	0.51	0.48			
Neoprene	0.50	0.44	0.54	0.56	0.50	0.53	0.56	0.51	0.54	0.57	0.51	0.49	0.53	(0.51)	0.52	-	0.54	0.57	0.52	0.44	0.52	0.21	0.40	(0.48)	0.46	0.50	0.52	0.44	0.52	0.21	0.40	(0.48)	0.46	0.50	0.52	0.44	0.52	0.21	0.40	(0.48)	0.46	
Cotton	0.52	0.59	0.49	0.55	0.52	0.49	0.52	0.50	0.53	0.59	0.51	0.45	0.57	0.59	0.48	(0.53)	0.59	0.61	0.43	0.54	0.35	(0.43)	0.16	0.29	0.51	0.50	0.55	0.55	0.39	(0.40)	0.19	0.33	0.20	0.51	0.50	0.55	0.39	(0.40)	0.19	0.33	0.20	
PU	0.53	0.58	0.47	0.59	0.48	0.51	0.54	0.57	0.53	0.60	0.51	0.53	0.52	0.56	0.52	(0.52)	0.58	0.56	0.55	0.55	0.39	(0.40)	0.19	0.33	0.20	0.51	0.55	0.55	0.39	(0.40)	0.19	0.33	0.20	0.51	0.55	0.55	0.39	(0.40)	0.19	0.33	0.20	
Cotton	0.44	0.54	0.50	0.51	0.49	0.50	0.47	0.48	0.50	0.52	0.47	0.48	0.51	-	0.41	-	0.36	0.50	0.50	0.43	0.47	0.38	0.37	0.40	0.38	0.43	0.44	0.50	0.47	0.38	0.37	0.40	0.38	0.43	0.44	0.50	0.47	0.38	0.37	0.40	0.38	
CSPE	0.43	0.54	0.50	0.40	0.50	0.43	0.46	0.46	0.53	0.49	0.44	0.50	0.48	-	0.47	-	0.48	0.52	0.39	0.47	0.46	0.34	0.47	0.43	0.50	0.42	0.43	0.39	0.47	0.46	0.34	0.47	0.43	0.50	0.42	0.43	0.39	0.47	0.46	0.34	0.47	0.43
Determinations made by	MW	JES	MW	MW	MW	MW	JES	JES	JES	JES	MW	MW	JES	JES	JES	JES	JES	JES	MW	MW	BM	BM	BM	BM	BM	BM	BM	MW	MW	BM	BM	BM	BM	BM	BM	BM	BM	BM	BM	BM	BM	

() specimen broke during exposure but pieces were recovered
 - specimen broke during exposure and pieces were lost
 Duplicate results in each cell refer to replication

Table 3
ERROR VARIANCES AND COEFFICIENTS OF VARIATION

	Set								
	a	b	c	d	e	f	g	h	i
Error variance of breaking strength	2.64×10^{-3}	2.16×10^{-3}	3.58×10^{-3}	3.13×10^{-3}	2.18×10^{-3}	2.55×10^{-3}	2.38×10^{-3}	4.74×10^{-3}	5.88×10^{-3}
Set mean strength, kN	0.91	0.86	0.82	0.69	0.85	0.88	0.86	0.81	1.08
Coefficient of variation of strength, %	5.7	5.4	7.3	8.1	5.5	5.7	5.7	8.5	7.1
Error variance of breaking extension	0.789	0.758	1.023	0.806	0.659	0.888	0.609	1.339	1.520
Set mean extension, %	15.6	13.6	14.0	10.4	13.3	14.9	14.7	14.0	17.8
Coefficient of variation of extension, %	5.1	5.6	7.3	7.8	5.0	6.0	4.2	9.6	8.5
Degrees of freedom in error	16	48	96	48	64	48	48	48	72

Table 4

ANALYSIS OF VARIANCE OF BREAKING STRENGTH

Factor	No. of degrees of freedom	No. of levels	No. of results per level	Variance ratios for set									
				(a) Controls	(b) 3 months	(c) 1% Natural rubber	(d) ERDM	(e) ERDM, 1%, with controls	(f) Cloncurry, 1%, with controls	(g) Immisfail, 1%, with controls	(h) Wylon with 3 rubbers		
Fabric F	1	2	16	2109	6347	6810	2362	8103	6107	5492	2608	-	
	1	2	48									-	
	1	2	64									-	
	1	2	96									-	
Rubber R	2	3	48	9.5	49.4	15.5	-	205	35.3	31.9	1.8	72.5	
	3	4	8										-
	3	4	24										-
	3	4	32										-
Time T	1	2	16	7.8	-	-	68.7	36.0	-	-	-	66.1	
	3	4	24										-
	3	4	32										-
	3	4	36										-
Load L	1	2	48	-	21.6	-	301.5	21.3	-	-	-	110.9	
	1	2	64										-
	1	2	72										-
	1	2	96										-
Site S	2	3	32	-	12.7	59.6	1.2	-	-	-	-	42.7	
	2	3	48										-
	2	3	64										-
	2	3	96										-
FR	3	8	4	3.1	22.8	24.9	-	30.8	15.2	11.0	6.7	-	
	3	8	12									-	
	3	8	16									-	
	3	8	24									-	
FT	1	4	8	2.2	-	-	14.7	5.5	-	-	-	-	
	3	8	12									-	
	3	8	16									-	
	3	8	24									-	
FL	1	4	24	-	29.6	-	272.7	34.0	-	-	-	-	
	1	4	32									-	
	1	4	48									-	
	1	4	72									-	
FS	2	6	16	-	8.3	21.9	24.7	-	-	-	-	-	
	2	6	32									-	
	2	6	48									-	
	2	6	72									-	
RT	3	8	4	0.4	-	-	-	16.7	-	-	-	3.1	
	6	12	12										-
	9	16	8										-
	9	16	12										-
RL	2	6	24	-	21.6	-	-	39.6	-	-	-	98.6	
	3	8	12										-
	3	8	16										-
	3	8	24										-
RS	4	9	16	-	1.2	14.5	-	-	-	-	-	2.7	
	6	12	8										-
	6	12	16										-
	6	12	24										-
TL	3	8	12	-	-	-	0.6	0.9	-	-	-	0.6	
	3	8	16										-
	3	8	18										-
	3	8	24										-
TS	6	12	8	-	-	5.7	6.6	-	-	-	-	5.9	
	6	12	12										-
	6	12	16										-
	6	12	24										-
LS	2	6	16	-	1.0	-	0.2	-	-	-	-	8.1	
	2	6	24										-
	2	6	32										-
	2	6	48										-
FRT	3	16	2	0.4	-	2.6	-	1.5	-	-	-	-	
	9	32	4									-	
	9	32	6									-	
	15	48	2									-	
FRL	3	16	6	-	21.6	-	-	32.2	-	-	-	-	
	3	16	8									-	
	3	16	12									-	
	3	16	16									-	
FRS	6	24	4	-	2.4	0.3	-	-	-	-	-	-	
	6	24	8									-	
	6	24	12									-	
	6	24	16									-	
FTL	3	16	6	-	-	-	0.3	1.8	-	-	-	-	
	3	16	8									-	
	3	16	12									-	
	3	16	16									-	
FTS	6	24	4	-	-	2.8	1.5	-	-	-	-	-	
	6	24	8									-	
	6	24	12									-	
	6	24	16									-	
FLS	2	12	8	-	0.3	-	4.4	-	-	-	-	-	
	2	12	12									-	
	2	12	16									-	
	2	12	24									-	
RTL	6	24	6	-	-	-	-	2.1	-	-	-	1.9	
	6	24	8										-
	6	24	12										-
	6	24	16										-
RTS	12	36	4	-	-	3.7	-	-	-	-	-	2.7	
	18	48	4										-
	18	48	6										-
	18	48	8										-
TLS	6	24	4	-	-	-	1.5	-	-	-	-	1.3	
	6	24	8										-
	6	24	12										-
	6	24	16										-
LSR	4	18	8	-	1.0	-	-	-	-	-	-	0.3	
	4	18	12										-
	4	18	16										-
	4	18	24										-
FRTL	9	64	2	-	-	-	-	1.4	-	-	-	-	
	9	64	4									-	
	9	64	6									-	
	9	64	8									-	
FRS	18	96	2	-	-	0.6	-	-	-	-	-	-	
	18	96	4									-	
	18	96	6									-	
	18	96	8									-	
FTLS	6	48	2	-	1.2	-	-	-	-	-	-	-	
	6	48	4									-	
	6	48	6									-	
	6	48	8									-	
FTLS	6	48	2	-	-	-	0.5	-	-	-	-	-	
	6	48	4									-	
	6	48	6									-	
	6	48	8									-	
RTLS	12	72	2	-	-	-	-	-	-	-	-	2.1	
	12	72	4										-
	12	72	6										-
	12	72	8										-

- No determination possible in this set

BEST AVAILABLE COPY

ANALYSIS OF VARIANCE OF BREAKING EXTENSION

Factor	No. of degrees of freedom	No. of levels	No. of results per level	Variance ratios for set										
				(a) Controls	(b) 3 months	(c) IX	(d) Natural rubber	(e) ERDE	(f) ERDE, IX, with controls	(g) Cloncurry, IX, with controls	(h) Innisfail, IX, with controls	(i) Nylon with 3 rubbers		
Fabric F	1	2	16	1598	5457	7035	3286	7570	4223	5534	2891	-		
	1	2	48									-		
	1	2	64									-		
	1	2	96									-		
Rubber R	2	3	48	21.9	43.2	49.1	-	186	52.2	77.1	12.7	114.6		
	3	4	8									-		
	3	4	24									-		
	3	4	32									-		
Time T	1	2	16	51.6	-	-	50.2	19.1	-	-	-	56.8		
	3	4	24										-	
	3	4	32										-	
	3	4	36										-	
	3	4	48										45.2	
Load L	1	2	48	-	308	-	674	325	-	-	-	305		
	1	2	64	-	-	-	-		-	-				
	1	2	72	-	-	-	-		-	-				
Site S	2	3	32	-	0.4	37.0	4.1	-	-	-	-	20.9		
	2	3	48	-	-		-	-	-	-				
	2	3	64	-	-		-	-	-	-				
FR	3	8	4	3.8	4.1	6.7	-	20.8	3.3	11.5	2.9	-		
	3	8	12				-					-	-	
	3	8	16				-					-	-	
FT	1	4	8	0.1	-	5.3	11.0	9.6	-	-	-	-		
	3	8	12									-	-	-
	3	8	16									-	-	-
	3	8	20									-	-	-
	5	12	8									-	-	-
FL	1	4	24	-	0.3	-	106.4	0.1	-	-	-	-		
	1	4	32	-	-	-	-		-	-	-			
FS	2	6	16	-	12.1	6.9	11.4	-	-	-	-	-		
	2	6	32	-	-		-	-	-	-	-			
FX	3	8	4	1.5	-	3.6	-	7.6	-	-	-	2.3		
	6	12	12				-						-	-
	9	16	8				-						-	-
	9	16	12				-						-	-
	15	24	5				-						-	-
RL	2	6	24	-	-	-	-	-	-	-	-	57.9		
	3	8	12	-	12.8	-	-	-	-	-	-			
	3	8	16	-	-	-	20.6	-	-	-	-			
RS	4	9	16	-	-	-	-	-	-	-	-	5.6		
	6	12	8	-	2.9	-	-	-	-	-	-			
	6	12	16	-	-	12.6	-	-	-	-	-			
TL	3	8	12	-	-	-	0.9	2.7	-	-	-	2.3		
	3	8	16	-	-	-	-		-	-	-			
	3	8	18	-	-	-	-		-	-	-			
TS	6	12	8	-	-	-	3.0	-	-	-	-	5.3		
	6	12	12	-	-	-	-	-	-	-	-			
	6	12	16	-	-	4.7	-	-	-	-	-			
LS	2	6	16	-	0.2	-	1.3	-	-	-	-	5.5		
	2	6	24	-	-	-	-	-	-	-	-			
FRT	3	16	2	0.1	-	-	-	2.5	-	-	-	-		
	9	32	4		-	-	-					-		
	9	32	6		-	3.8	-					-	-	
	15	48	2		-	-	-					2.7	2.3	1.1
FRL	3	16	6	-	19.2	-	-	17.8	-	-	-	-		
	3	16	8	-	-	-	-		-	-	-	-		
FRS	6	24	4	-	2.9	-	-	-	-	-	-	-		
	6	24	8	-	-	3.0	-	-	-	-	-	-		
FTL	3	16	6	-	-	-	2.2	7.4	-	-	-	-		
	3	16	8	-	-	-	-		-	-	-	-		
FTS	6	24	4	-	-	-	0.6	-	-	-	-	-		
	6	24	8	-	-	3.2	-	-	-	-	-	-		
FLS	2	12	8	-	1.3	-	0.5	-	-	-	-	-		
				-					-	-	-	-		
RTL	6	24	6	-	-	-	-	2.2	-	-	-	3.4		
	9	32	4	-	-	-	-		-	-	-		-	
RTS	12	36	4	-	-	2.2	-	-	-	-	-	2.5		
	18	36	4	-	-	-	-	-	-	-	-		-	
TLS	6	24	4	-	-	-	2.0	-	-	-	-	0.9		
	6	24	6	-	-	-	-	-	-	-	-		-	
LSR	4	18	8	-	-	-	-	-	-	-	-	1.8		
	6	24	4	-	0.3	-	-	-	-	-	-		-	
FRTL	9	64	2	-	-	-	-	2.6	-	-	-	-		
				-						-	-	-	-	
FRTS	18	96	2	-	-	1.0	-	-	-	-	-	-		
				-					-	-	-	-		
FRLS	6	48	2	-	1.9	-	-	-	-	-	-	-		
				-					-	-	-	-		
FTLS	6	48	2	-	-	-	0.9	-	-	-	-	-		
				-					-	-	-	-		
RTLS	12	72	2	-	-	-	-	-	-	-	-	1.7		
				-					-	-	-		-	

- No determination possible in this set

Table 6

TABLE OF SIGNIFICANT MEAN BREAKING STRENGTHS, kN

Factor	Level	Set (see Table 4)									
		(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)	
F	Nylon Cotton	1.32 0.49	1.24 0.49	1.18 0.46	0.97 0.41	1.22 0.48	1.28 0.48	1.23 0.49	1.16 0.45	1.08	
R	Natural Neoprene PU CSPE	0.88 0.84 0.98 0.92	0.79 0.87 0.95 0.85	0.79 0.81 0.87 0.81	0.69	0.68 0.88 0.96 0.86	0.82 0.86 0.96 0.89	0.84 0.83 0.94 0.83	0.82 0.78 0.81 0.82	0.97 1.13 1.14	
T	Original Final 3 months 6 months 12 months 65 months	0.88 0.93	0.86	0.89 0.82 0.74 0.84	0.79 0.71 0.56 0.70	0.90 0.83 0.79 0.88	0.88 0.93 0.91 0.86 0.80 0.90	0.88 0.93 0.87 0.87 0.74 0.87	0.88 0.93 0.88 0.73 0.67 0.74	1.19 1.08 0.94 1.10	
L	1X 10X		0.89 0.84	0.82	0.79 0.59	0.87 0.83	0.88	0.86	0.81	1.14 1.01	
S	ERDE Cloucurry Imisfail		0.90 0.84 0.86	0.87 0.84 0.76	0.68 0.70 0.69	0.85	0.88	0.86	0.81	1.16 1.03 1.04	
FR	Natural Neoprene PU CSPE	Nylon Cotton 1.34 0.44 1.22 0.47 1.40 0.56 1.34 0.49	Nylon Cotton 1.12 0.46 1.22 0.51 1.39 0.51 1.23 0.47	Nylon Cotton 1.16 0.42 1.11 0.51 1.27 0.46 1.16 0.46	Nylon Cotton 1.12 0.46 0.99 0.43 0.79 0.34 0.96 0.44	Nylon Cotton 1.01 0.35 1.23 0.54 1.40 0.53 1.24 0.48	Nylon Cotton 1.25 0.38 1.21 0.51 1.40 0.52 1.28 0.49	Nylon Cotton 1.22 0.46 1.15 0.50 1.35 0.54 1.20 0.46	Nylon Cotton 1.20 0.44 1.09 0.47 1.20 0.42 1.18 0.46		
FT	Original Final 3 months 6 months 12 months 65 months	1.31 0.45 1.34 0.53		1.29 0.48 1.16 0.48 1.05 0.42 1.20 0.47	1.12 0.46 0.99 0.43 0.79 0.34 0.96 0.44	1.30 0.50 1.19 0.47 1.15 0.43 1.24 0.52	1.31 0.45 1.34 0.53 1.24 0.47 1.17 0.43 1.30 0.50	1.31 0.45 1.34 0.53 1.25 0.49 1.22 0.52 1.02 0.46 1.24 0.50	1.31 0.45 1.34 0.53 1.28 0.48 1.02 0.45 0.97 0.36 1.07 0.42		
FL	1X 10X		1.29 0.48 1.20 0.49		1.16 0.42 0.78 0.41	1.26 0.47 1.18 0.48					
FS	ERDE Cloucurry Imisfail		1.30 0.50 1.19 0.49 1.24 0.48	1.26 0.47 1.18 0.40 1.09 0.43	1.01 0.35 0.94 0.47 0.96 0.42						
EL	Natural Neoprene PU CSPE	1X 10X 0.88 0.70 0.87 0.86 0.95 0.96 0.90 0.89			1X 10X 0.78 0.59 0.86 0.90 0.95 0.97 0.87 0.85					1X 10X 1.16 0.78 1.12 1.14 1.16 1.12	
LS	ERDE Cloucurry Imisfail		0.91 0.88 0.87 0.81 0.88 0.84		0.78 0.59 0.81 0.60 0.78 0.59					1.22 1.10 1.13 0.93 1.08 1.00	

Table 6 (continued)

RT		Original	Final	3 months	6 months	12 months	65 months
(a)	Natural	0.88	0.91				
	Neoprene	0.82	0.86				
	PU	0.95	1.00				
	CSPE	0.88	0.96				
(c)	Natural			0.88	0.82	0.67	0.80
	Neoprene			0.87	0.83	0.71	0.84
	PU			0.95	0.84	0.80	0.88
	CSPE			0.86	0.79	0.76	0.83
(e)	Natural			0.82	0.70	0.48	0.74
	Neoprene			0.89	0.86	0.87	0.92
	PU			0.98	0.95	0.94	0.99
	CSPE			0.90	0.81	0.86	0.87
(f)	Natural	0.88	0.91	0.92	0.81	0.58	0.80
	Neoprene	0.82	0.86	0.88	0.86	0.82	0.90
	PU	0.95	1.00	0.95	0.93	0.96	0.98
	CSPE	0.88	0.96	0.90	0.84	0.84	0.90
(g)	Natural	0.88	0.91	0.88	0.84	0.68	0.83
	Neoprene	0.82	0.86	0.85	0.88	0.68	0.90
	PU	0.95	1.00	0.95	0.93	0.86	0.97
	CSPE	0.88	0.96	0.80	0.81	0.74	0.80
(h)	Natural	0.88	0.91	0.84	0.80	0.74	0.76
	Neoprene	0.82	0.86	0.87	0.75	0.63	0.74
	PU	0.95	1.00	0.94	0.67	0.58	0.70
	CSPE	0.88	0.96	0.86	0.71	0.72	0.78
(i)	Natural			1.13	0.90	0.79	0.97
	Neoprene			1.22	1.15	0.99	1.15
	PU						
	CSPE			1.23	1.10	1.04	1.17

Table 6 (concluded)

RS		(b)			(c)			(d)	(e)	(i)	
		ERDE	Cloncurry	Innisfail	ERDE	Cloncurry	Innisfail			ERDE	Cloncurry
TS	Natural	0.82	0.78	0.78	0.78	0.81	0.78			1.01	0.94
	Neoprene	0.89	0.85	0.86	0.86	0.82	0.75			1.23	1.09
	PU	0.98	0.94	0.95	0.95	0.93	0.72			1.24	1.08
	CSPE	0.90	0.79	0.86	0.87	0.79	0.77			1.25	1.13
FEL	3 months				0.91	0.87	0.88	0.82	0.78	1.13	1.01
	6 months				0.86	0.87	0.73	0.69	0.73	1.08	0.83
	12 months				0.80	0.74	0.67	0.48	0.59	1.18	1.08
	68 months				0.90	0.87	0.74	0.74	0.71	1.03	
	Natural	Natural	Neoprene	PU	CSPE						
	Nylon 12	1.30	1.22	1.40	1.25						
	Nylon 10Z	0.95	1.23	1.39	1.22						
	Cotton 12	0.46	0.52	0.49	0.47						
	Cotton 10Z	0.46	0.50	0.54	0.47						

Natural = natural rubber
 PU = polyurethane
 CSPE = chlorosulphonated polyethylene

Table 7

TABLE OF SIGNIFICANT MEAN BREAKING EXTENSIONS, PER CENT

Set (see Table 4)										
Factor	Level	(a)	(b)	(c)	(d)	(e)	(f)	(g)	(h)	(i)
F	Nylon Cotton	21.9 9.3	20.2 7.1	20.1 7.9	15.7 5.2	19.5 7.1	21.2 8.7	20.6 8.8	20.3 7.6	17.8
R	Natural Neoprene PU CSPE	14.7 14.0 17.2 16.4	12.1 13.5 14.9 14.1	12.8 13.6 15.2 14.4		10.5 13.6 15.1 13.9	13.4 14.5 16.7 15.2	12.6 13.5 16.5 15.1	13.3 13.2 14.4 14.9	15.7 18.5 19.3
T	Original Final 3 months 6 months 12 months 6S months	14.5 16.7	13.6	13.2 13.9 12.8 14.1	12.1 10.4 8.9 10.3	13.7 13.2 12.5 13.8	14.5 16.7 15.4 15.1	14.5 16.7 15.1 14.1	14.5 16.7 15.1 13.0	19.8 17.8 16.0 17.8
L	IX 10X		15.2 12.1	14.0	12.8 8.1	14.6 12.0	14.9	14.7	14.0	19.6 16.0
S	ERDE Cloncurry Imisfail		13.7 13.5 13.6	14.6 14.2 13.1	10.5 10.7 10.1	13.3	14.9	14.7	14.0	18.7 17.1 17.8
FR	Natural Neoprene PU CSPE	Nylon Cotton 20.8 8.7 18.2 6.0 19.7 8.4 23.5 10.9 23.6 9.3	Nylon Cotton 18.2 6.0 20.2 6.8 21.9 7.9 20.5 7.6	Nylon Cotton 19.0 6.6 19.2 7.9 21.8 8.6 20.4 8.4	Nylon Cotton 16.3 4.8 20.2 7.1 22.1 8.1 19.6 8.3	Nylon Cotton 16.3 4.8 20.2 7.1 22.1 8.1 19.6 8.3	Nylon Cotton 19.8 6.9 20.4 8.5 23.3 10.0 21.2 9.2	Nylon Cotton 19.5 7.8 18.7 8.3 22.7 10.3 21.6 8.7	Nylon Cotton 19.5 7.2 19.1 7.3 21.0 7.8 21.7 8.2	
FT	Original Final 3 months 6 months 12 months 6S months	20.7 8.2 23.0 10.4		21.7 8.7 19.7 8.1 18.7 6.9 20.4 7.8	18.2 6.0 15.5 5.3 13.7 4.2 15.3 6.7		20.7 8.2 23.0 10.4 22.3 8.4 20.2 8.6 19.3 7.7 21.5 8.7	20.7 8.2 23.0 10.4 20.9 9.4 20.8 8.7 18.2 7.8 20.1 8.1	20.7 8.2 23.0 10.4 21.9 8.2 18.1 6.9 18.4 5.3 19.5 6.5	
FS	ERDE Cloncurry Imisfail		20.6 6.9 19.5 7.6 20.5 6.7	20.8 8.4 20.0 8.5 19.5 6.7	16.3 4.8 15.4 6.0 15.4 4.8					
BL	Natural Neoprene PU CSPE		IX 10X 14.6 9.6 14.8 12.3 16.1 13.7 15.3 12.8		IX 10X 12.7 8.4 14.7 12.6 16.4 13.8 14.6 13.3					IX 10X 19.0 12.4 19.2 17.7
LS	ERDE Cloncurry Imisfail		15.4 12.1 15.1 12.0 15.1 12.1		12.7 8.4 13.1 8.3 12.6 7.5					20.6 18.0 20.0 17.3 19.2 14.9 19.6 15.9
PL	Nylon Cotton		21.7 18.7 8.7 5.5		19.0 12.4 6.6 3.8	20.8 18.3 8.4 5.8				

Table 7 (continued)

RT		Original	Final	3 months	6 months	12 months	6S months
(a)	Natural	14.1	15.3				
	Neoprene	12.7	15.4				
	PU	16.0	18.4				
	CSPE	15.0	17.9				
(c)	Natural			14.6	13.0	11.1	12.6
	Neoprene			14.8	13.8	11.7	14.0
	PU			16.1	15.0	14.4	15.2
	CSPE			15.3	13.9	14.0	14.4
(e)	Natural			12.4	10.3	8.4	11.0
	Neoprene			13.8	13.6	12.9	14.2
	PU			15.2	15.1	14.5	15.7
	CSPE			13.6	13.8	14.1	14.4
(f)	Natural	14.1	15.3	14.9	13.0	10.0	12.8
	Neoprene	12.7	15.4	15.1	14.6	13.5	15.4
	PU	16.0	18.4	16.5	16.1	16.1	17.0
	CSPE	15.0	17.9	14.9	13.8	14.5	15.1
(g)	Natural	14.1	15.3	14.9	13.6	11.2	12.8
	Neoprene	12.7	15.4	14.1	13.8	11.1	13.9
	PU	16.0	18.4	16.0	16.8	15.9	15.8
	CSPE	15.0	17.9	15.5	14.8	13.8	13.9
(h)	Natural	14.1	15.3	14.0	12.2	12.0	12.2
	Neoprene	12.7	15.4	15.0	12.9	10.4	12.8
	PU	16.0	18.4	15.8	12.0	11.4	12.8
	CSPE	15.0	17.9	15.6	13.0	13.7	14.3
(i)	Natural			18.2	15.5	13.7	15.3
	Neoprene			20.2	19.0	16.2	18.5
	PU						
	CSPE			20.9	18.8	18.1	19.5

Table 7 (concluded)

RS		(b) ERDE Cloncurry Innisfail	(c) ERDE Cloncurry Innisfail	(d) ERDE Cloncurry Innisfail	(e)	(f) ERDE Cloncurry Innisfail
	Natural Neoprene PU CSPE	12.4 12.2 11.7 13.8 12.8 14.0 15.2 14.9 14.4 13.6 14.3 14.3	12.7 13.1 12.6 14.7 13.2 12.7 16.4 16.1 13.0 14.6 14.5 14.2			16.3 15.4 15.4 20.2 17.0 18.3
TS	3 months 6 months 12 months 6S months		15.4 15.1 15.1 14.4 14.8 12.5 13.5 13.0 11.9 15.1 14.1 13.0	12.4 12.2 11.7 10.3 11.2 9.8 8.4 9.3 9.1 11.0 10.1 9.7		19.6 18.8 19.6 19.9 18.8 20.7 18.6 17.9 16.8 17.4 14.6 16.0 18.8 17.0 17.5
FTL	Nylon 12 Nylon 10Z Cotton 12 Cotton 10Z	Natural Neoprene PU CSPE 21.8 20.8 22.5 21.8 14.7 19.7 21.2 19.2 7.4 8.7 9.7 8.8 4.5 4.9 6.1 6.4			Natural Neoprene PU CSPE 19.3 20.7 23.3 20.0 13.2 19.6 21.0 19.2 6.1 8.6 9.6 9.1 3.5 5.5 6.6 7.4	
FTL	Nylon 12 Nylon 10Z Cotton 12 Cotton 10Z			3 6 12 6S mths mths mths mths 21.8 18.6 17.1 18.6 14.7 12.4 10.3 12.1 7.4 7.3 5.1 6.7 4.5 3.4 3.2 4.0	3 6 12 6S mths mths mths mths 22.3 20.2 19.3 21.5 18.8 18.9 17.2 18.2 8.4 8.6 7.7 8.7 5.4 5.1 5.6 6.9	

Natural = natural rubber
 PU = polyurethane
 CSPE = chlorosulphonated polyethylene

REFERENCES

<u>No.</u>	<u>Author</u>	<u>Title, etc</u>
1	J.E. Swallow M. Webb	The flexibility of weathered rubber-coated fabrics. RAE Technical Report 77016 (1977)
2	British Standards Institution	Inspection and testing of textiles. BS 3F 100 (1975)
3	J.E. Swallow	Effects of dyes and finishes on the weathering of nylon textiles. RAE Technical Report 74179 (1975)

REPORT DOCUMENTATION PAGE

Overall security classification of this page

UNCLASSIFIED

As far as possible this page should contain only unclassified information. If it is necessary to enter classified information, the box above must be marked to indicate the classification, e.g. Restricted, Confidential or Secret.

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16. Descriptors (Keywords) (Descriptors marked * are selected from TEST) Rubber-coated fabrics. Weathering. Strength. Extension					
17. Abstract ↓ The breaking strength and extension of a nylon and of a cotton fabric, each coated with natural rubber, neoprene, polyurethane or chlorosulphonated polyethylene and exposed to various weathering conditions, were determined. Although the coated nylon fabrics were stronger and more extensible than the cotton ones, those with natural rubber coating deteriorated at a faster rate when exposed under load. Nylon coated with polyurethane was initially stronger and more extensible than when coated with the other rubbers, but in hot moist weathering conditions deteriorated faster. Extension was more severely affected than strength by load during exposure. ↖					

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